

# What is *planar* splitting?

[Review of the Method of Characteristics](#) (MoC; Stone & Norman, 1992):

- first successful attempt to upwind an MHD code (3 of 7 characteristics).
- Basic principle: *compressional* terms can be “operator split” from the *transverse* terms.

MHD equations:

$$\partial_t \rho + \nabla \cdot (\rho \vec{v}) = 0; \quad (1)$$

$$\partial_t e + \nabla \cdot (e \vec{v}) = -p \nabla \cdot \vec{v} \quad (2)$$

$$\partial_t \vec{v} + \vec{v} \cdot \nabla \vec{v} = \frac{1}{\rho} \left( -\nabla p^* + (\vec{B} \cdot \nabla) \vec{B} \right); \quad (3)$$

$$\partial_t \vec{B} + \nabla (\vec{B} \vec{v}) = \nabla (\vec{v} \vec{B}), \quad (4)$$

where  $p = (\gamma - 1)e$  and  $p^* = p + B^2/2$ .  $\vec{B}$  is in units where  $\mu_0 = 1$ .

Written out in components (with 3-symmetry assumed):

$$\partial_t \rho + \partial_1 \rho v_1 + \partial_2 \rho v_2 = 0; \quad (5)$$

$$\partial_t e + \partial_1 e v_1 + \partial_2 e v_2 = -p \nabla \cdot \vec{v}; \quad (6)$$

$$\partial_t v_1 + v_1 \partial_1 v_1 + v_2 \partial_2 v_1 = -\frac{1}{\rho} \partial_1 p^* + \frac{1}{\rho} B_1 \partial_1 B_1 + \frac{1}{\rho} B_2 \partial_2 B_1; \quad (7)$$

$$\partial_t v_2 + v_1 \partial_1 v_2 + v_2 \partial_2 v_2 = -\frac{1}{\rho} \partial_2 p^* + \frac{1}{\rho} B_1 \partial_1 B_2 + \frac{1}{\rho} B_2 \partial_2 B_2; \quad (8)$$

$$\partial_t B_1 + v_1 \partial_1 B_1 + v_2 \partial_2 B_1 = -B_1 \nabla \cdot \vec{v} + B_1 \partial_1 v_1 + B_2 \partial_2 v_1; \quad (9)$$

$$\partial_t B_2 + v_1 \partial_1 B_2 + v_2 \partial_2 B_2 = -B_2 \nabla \cdot \vec{v} + B_1 \partial_1 v_2 + B_2 \partial_2 v_2, \quad (10)$$

where **blue** terms are *compressive*, **red** terms are *transverse* (cross-derivatives).

Examining only the transverse terms for  $v_2$  and  $B_2$  [equations (8) and (10)]:

$$\partial_t v_2 + v_1 \partial_1 v_2 = a_1 \partial_1 a_2; \quad (11)$$

$$\partial_t a_2 + v_1 \partial_1 a_2 = a_1 \partial_1 v_2, \quad (12)$$

where  $a_i = B_i/\sqrt{\rho}$  is the Alfvén speed. Adding and subtracting (11) and (12):

$$\partial_t v_2 + (v_1 - a_1) \partial_1 v_2 + \partial_t a_2 + (v_1 - a_1) \partial_1 a_2 = 0; \quad (13)$$

$$\partial_t v_2 + (v_1 + a_1) \partial_1 v_2 - \partial_t a_2 - (v_1 + a_1) \partial_1 a_2 = 0. \quad (14)$$

*characteristic speeds:*  $c_i^\pm = v_i \mp a_i$ ;

*Lagrangian derivatives:*  $D_{t,i}^\pm = \partial_t + c_i^\pm \partial_i \Rightarrow$

$$D_{t,1}^+ v_2 + D_{t,1}^+ a_2 = 0 \Rightarrow D_{t,1}^+ c_2^- = 0; \quad (15)$$

$$D_{t,1}^- v_2 - D_{t,1}^- a_2 = 0 \Rightarrow D_{t,1}^- c_2^+ = 0. \quad (16)$$

$\Rightarrow c_2^\mp$  is the *Riemann invariant* along *characteristic*  $\mathcal{C}_1^\pm$ .

Similarly,  $c_1^\mp$  is the Riemann invariant along characteristic  $\mathcal{C}_2^\pm$ .

Alternative form of the induction equation (4):

$$\partial_t \vec{B} = \nabla \times (\vec{v} \times \vec{B}) \equiv \nabla \times \vec{E}, \quad (17)$$

where  $\vec{E} = \vec{v} \times \vec{B}$  is the *induced electric field*. With 3-symmetry:

$$\partial_t B_1 = \partial_2 E_3; \quad \partial_t B_2 = -\partial_1 E_3, \quad (18)$$

where  $E_3 = v_1 B_2 - v_2 B_1$ .

Staggered mesh  $\Rightarrow$  scalars ( $\rho, e$ ) zone-centred;  
 primary vectors ( $\vec{v}, \vec{B}$ ) face-centred;  
 secondary vectors ( $\vec{E}$ ) edge-centred.

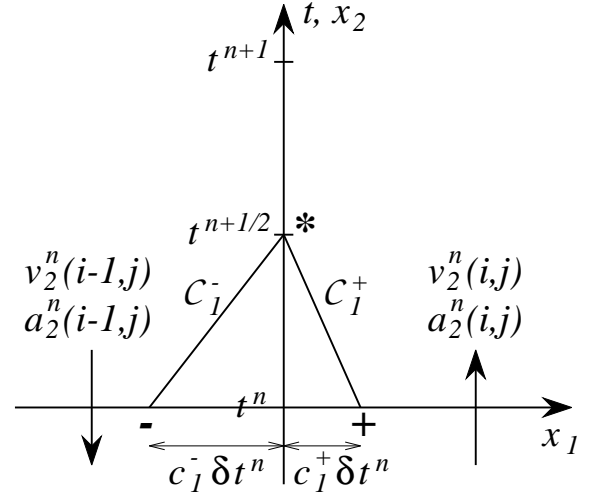
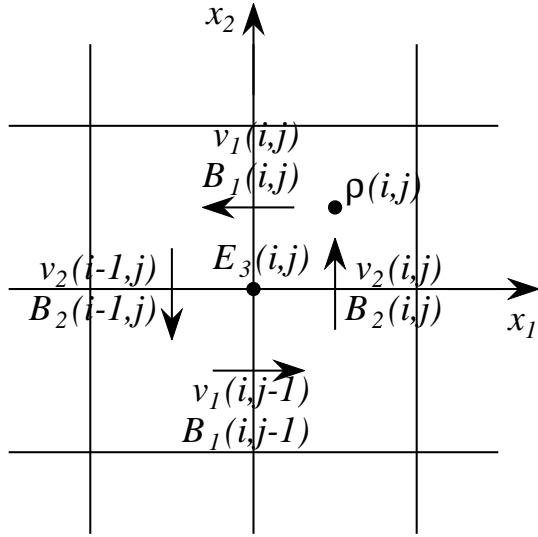
$\Rightarrow \partial_2 E_3$  ( $\partial_1 E_3$ ) co-spatial with  $B_1$  ( $B_2$ ),  $\partial_t(\nabla \cdot \vec{B}) = 0$  to machine accuracy.

For  $E_3$ , need time-centred, upwinded interpolations of  $v_1, v_2, B_1$ , and  $B_2$  to the 3-edges ( $v_1^*, v_2^*, B_1^*$ , and  $B_2^*$ ).

For  $v_2^*$  and  $B_2^*$ , construct a space-time diagram centred on the 3-edge with the 1-characteristics arriving at the 3-edge at  $t^{n+1/2}$  ( $t^*$ ).

Difference (15) along  $\mathcal{C}_1^+$  and (16) along  $\mathcal{C}_1^-$  to get:

$$(v_2^* + a_2^*) - (v_{2,+} + a_{2,+}) = 0; \quad (v_2^* - a_2^*) - (v_{2,-} - a_{2,-}) = 0, \quad (19)$$



where  $v_{2,\pm}$  and  $a_{2,\pm}$  are  $v_2$  and  $a_2$  interpolated to the bases of  $\mathcal{C}_1^\pm$  using the data at time  $t^n$ . Solve (19) for the “starred” quantities:

$$v_2^* = \frac{1}{2} (v_{2,+} + v_{2,-} + a_{2,+} - a_{2,-}); \quad a_2^* = \frac{1}{2} (a_{2,+} + a_{2,-} + v_{2,+} - v_{2,-}), \quad (20)$$

noting that  $B_2^* = \sqrt{\rho^*} a_2^*$ , with  $\rho^*$  some suitably centred value for  $\rho$ .

*To locate the bases of the characteristics, one needs preliminary guesses for  $c_1^\pm$  (call them  $\tilde{c}_1^\pm$ ). The original MoC used spatial averages:*

$$\tilde{c}_1^\pm = \frac{1}{2} (v_1(i, j) + v_1(i, j-1)) \mp \frac{1}{\sqrt{\rho^*}} \frac{1}{2} (B_1(i, j) + B_1(i, j-1)). \quad (21)$$

Repeat for  $v_1^*$  and  $B_1^*$ , then set:

$$E_3(i, j) = v_1^*(i, j) B_2^*(i, j) - v_2^*(i, j) B_1^*(i, j), \quad (22)$$

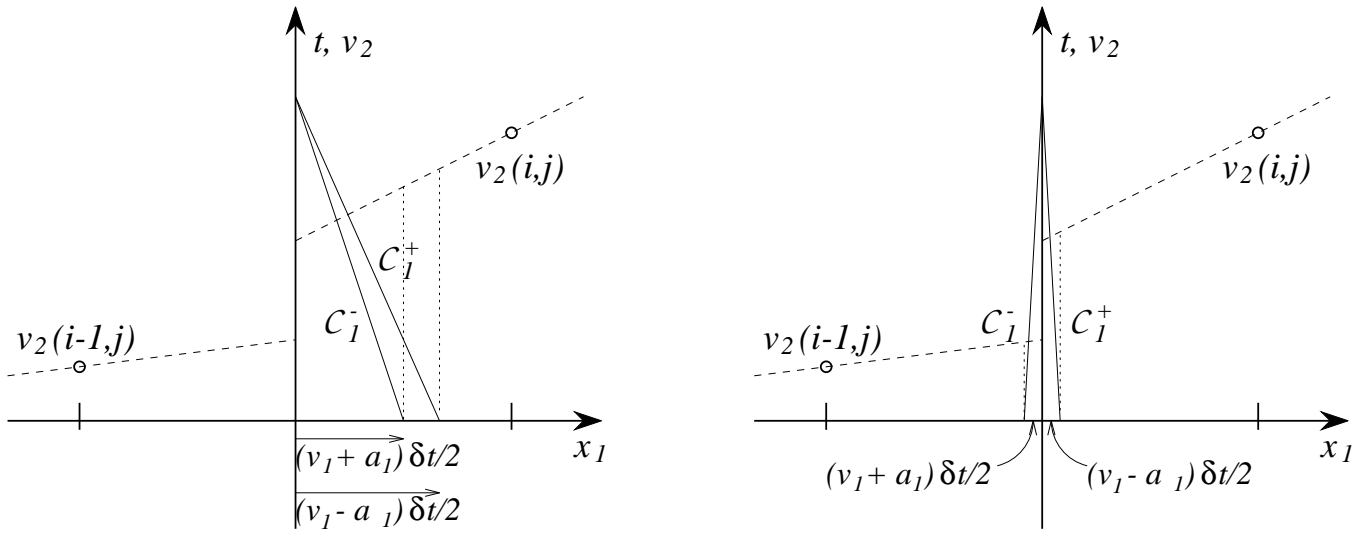
and use (18) to update  $B_1$  and  $B_2$ .

### Difficulty with super-Alfvénic turbulence

In general,  $v_1 \gg a_1 \Rightarrow \mathcal{C}_1^\pm$  on same side of zone boundary  $\Rightarrow v_{2,+} - v_{2,-} \propto a_1$ , and  $a_2^*$  remains  $\propto$  an *Alfvén* speed.

However, **and on occasion** (e.g., shear layer),

$$\begin{aligned} v_1(i, j) \approx -v_1(i, j-1) &\Rightarrow \tilde{v}_1(i, j) < \tilde{a}_1(i, j) \\ \Rightarrow \tilde{c}_1^\pm \text{ have opposite sign} &\Rightarrow \mathcal{C}_1^\pm \text{ straddle the zone boundary.} \end{aligned}$$

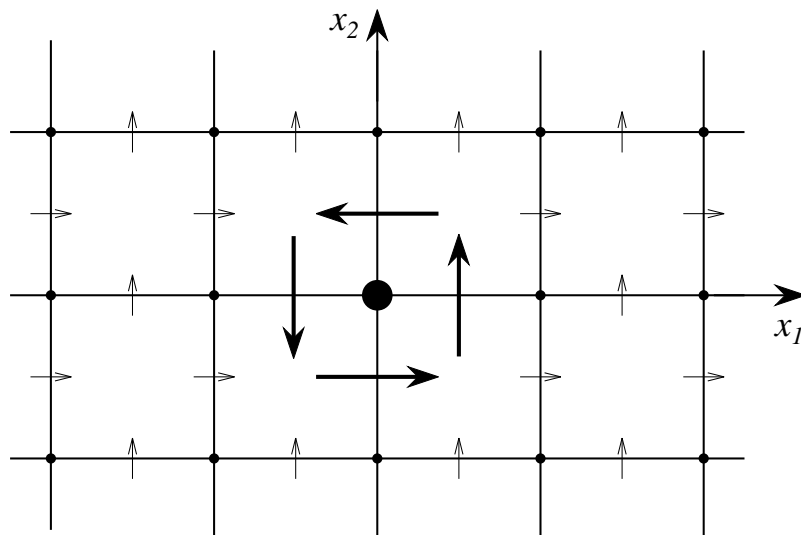


$\Rightarrow v_{2,+} - v_{2,-}$  contains the jump between the left and right interpolation functions  $\Rightarrow a_2^* \sim v_2$ , a flow speed.

This is not necessarily a bad thing!  $a_2^*$  ( $B_2^*$ ) appears only in (22) when  $E_3$  is evaluated. *If  $v_1^* \sim$  an Alfvén speed when  $a_2^* \sim$  a flow speed, the product  $v_1^* B_2^*$  can remain physical.*

Indeed, it was  $\tilde{v}_1 < \tilde{a}_1$  that caused  $C_1^\pm$  to straddle the zone boundary rendering  $a_2^* \sim v_2$  in the first place. **But  $v_1^* \neq \tilde{v}_1!$**  Even if  $\tilde{v}_1 < \tilde{a}_1$  (abnormal),  $v_1^* \sim$  a flow speed (normal).

$\Rightarrow E_3 \sim v_1 v_2 \Rightarrow$  the magnetic flux loop around the errant induced electric field has an Alfvén speed  $\sim$  a flow speed. This is a magnetic “explosion”.



## How frequent are explosions?

Let  $a_1/v_1 \sim 10^{-6}$ .  $\tilde{v}_1 < \tilde{a}_1 \Rightarrow v_1(i, j) + v_1(i, j-1) < 10^{-6}$  which happens once every  $\sim 10^6$  zone updates. For  $10^4$  time steps on a  $128^3$  grid  $\Rightarrow 20,000$  explosions, each injecting  $\sim 10^6$  times the original magnetic energy into the grid!

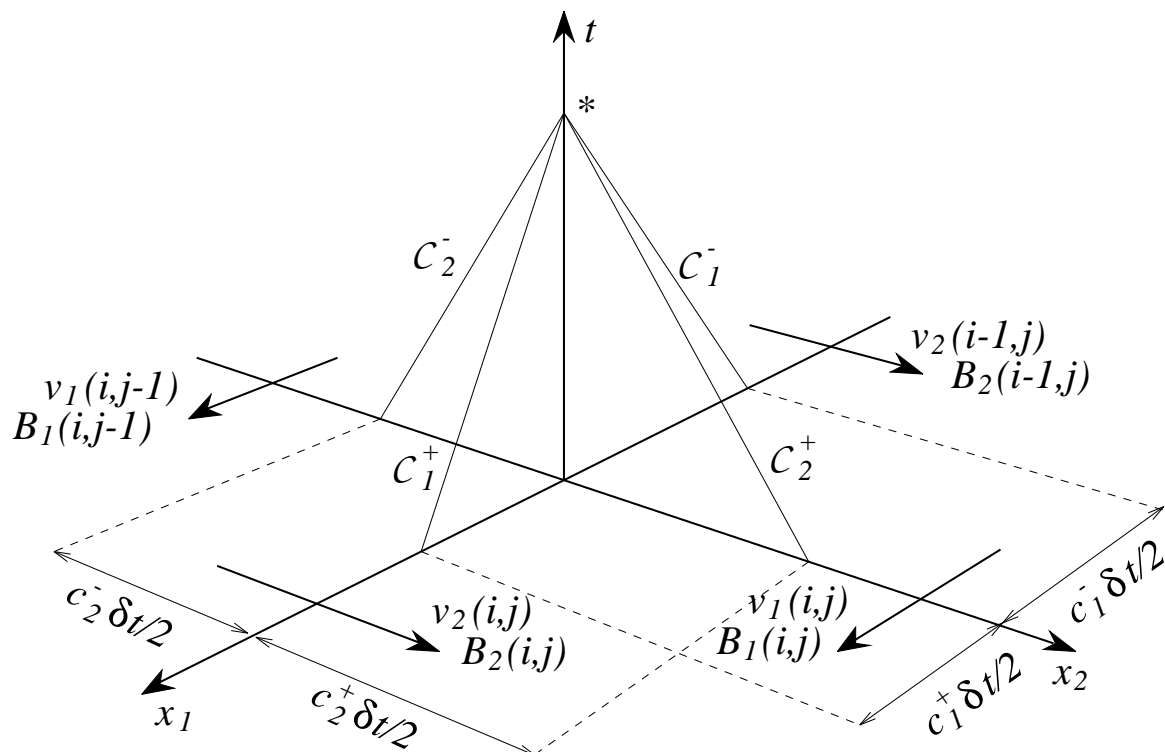
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## Planar Splitting

Locate bases of  $\mathcal{C}_1^\pm$  with  $v_1^*$  and  $a_1^*$  instead of  $\tilde{v}_1$  and  $\tilde{a}_1$ . Then, if  $v_1^* < a_1^*$  forces  $\mathcal{C}_1^\pm$  to straddle the zone boundary and  $a_2^* \sim v_2$ ,  $\Rightarrow v_1^* \sim a_1 \Rightarrow E_3 \sim v_1^* a_2^*$  remains well behaved. A “*virtual exchange*” of energies can be tolerated.

Problem:  $v_1^*$  and  $a_1^*$  require bases of  $\mathcal{C}_2^\pm$  to be set by  $v_2^*$  and  $a_2^*$ , and these can't be known until  $v_1^*$  and  $a_1^*$  are available to set the bases of  $\mathcal{C}_1^\pm$ !

This “catch-22” is solved by doing the interpolations *implicitly* on the 1-2 plane, identifying the “upwinded quadrant” instead of the traditional “upwinded direction”. This is *planar-splitting* (CMoC, Clarke 1996).



## Application to Godunov schemes

Directionally-split Godunov schemes [Ryu & Jones (1995), Dai & Woodward (1998), Falle *et al.* (1998)]:

- solve the seven-wave Riemann problem in each direction independently;
- account for discontinuities differently than MoC-based schemes and thus eliminate (?) “virtual exchanges” of kinetic and magnetic energies;
- set  $\partial_i B_i = 0$ , introducing directional biases (Gardiner & Stone, 2005);
- $\nabla \cdot \vec{B} = 0$  a problem.

Unsplit Godunov schemes [Balsara & Spicer (1999), Gardiner & Stone (2005), Ustyugov’s “PPM-L”]:

- include the  $\partial_i B_i$  terms;
- maintain  $\nabla \cdot \vec{B} = 0$  to machine accuracy;
- **susceptible to magnetic or kinetic explosions in sub-Alfvénic turbulence calculations** (Dave Collins, *private communication*).

Additional interpolations to compute  $\vec{E}$  from Riemann fluxes seem to make unsplit schemes vulnerable to virtual exchanges of kinetic and magnetic energies.

