

Assignment 1.

1. The apparent distance modulus of an object is given by:

$$V - M_V = 5 \log d - 5 + A_V$$

We are given that:  $d = 9.0 \text{ kpc} = 9000 \text{ pc}$

$$V = +13.0$$

$$M_V = -4.15$$

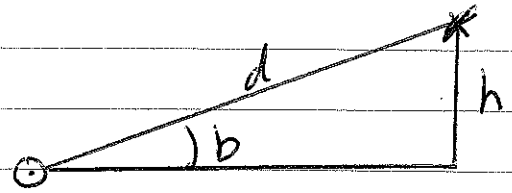
$$\begin{aligned} \therefore A_V &= (V - M_V) + 5 - 5 \log d \\ &= [13.0 - (-4.15)] + 5 - 5 \log_{10}(9000) \\ &= 22.15 - 5(3.9542425) \\ &= 22.15 - 19.77 \\ &= 2.38 \text{ magnitudes} \end{aligned}$$

a. The amount of visual interstellar extinction affecting UKS 2 is 2.38 magnitudes ( $A_V$ ).

b. The amount of extinction/kpc is  $2.38^m / 9 \text{ pc}$   
 $= 0.26^m / \text{kpc}$ .

That amount is somewhat small, given that values closer to  $1^m / \text{kpc}$  are more common along lines of sight in the plane of the Milky Way. UKS 2, however, is located in a line of sight lying slightly below the plane  $\sin \theta = -0.5 \text{ kpc} / 9.0 \text{ kpc} = -0.05555$   
 i.e.  $\theta = -3.18^\circ$ , which means it suffers less dust extinction, and probably all local, than other distant objects exactly in the Galactic plane.

2. The height of an object above the Galactic plane is established geometrically from its Galactic latitude  $b$  and distance  $d$  (see diagram) as:  $h = d \sin b$ .



$$\begin{aligned}\text{For M13, } b &= 40.9^\circ, \quad d = 7000 \text{ pc (7 kpc)} \\ \therefore h(\text{M13}) &= 7000 \text{ pc} \sin(40.9^\circ) \\ &= 7000 \text{ pc} \times 0.6547408 \\ &= 4583 \text{ pc}\end{aligned}$$

$$\begin{aligned}\text{For the Orion Nebula, } b &= -19.4^\circ, \quad d = 450 \text{ pc.} \\ \therefore h(\text{ON}) &= 450 \text{ pc} \sin(-19.4^\circ) \\ &= 450 \text{ pc} \times -0.3321611 \\ &= -149 \text{ pc.}\end{aligned}$$

The results indicate that the Orion Nebula qualifies as belonging to the Thin Disk, maximum heights above the plane of  $\sim 350 \text{ pc}$ , whereas M13 lies well outside the range of the Thick Disk, maximum heights above the plane of  $\sim 1000 \text{ pc}$ . M13 is therefore a member of the Galactic halo, and the Orion Nebula the thin disk.

3. The standard formula for escape speed in a Keplerian system is given by:  $v_{esc} = \sqrt{\frac{2GM_G}{R}}$ , where  $M_G$  is actually  $M_G + M_*$ .

$$\text{Take } G = 6.6726 \times 10^{-11} \text{ Nm}^2/\text{kg}^2$$

$$R = 8.5 \text{ kpc (locally)} = 8.5 \times 10^3 \times 206265 \times 1.4960 \times 10^{11} \text{ m} \\ = 2.6229 \times 10^{20} \text{ m}$$

$$(a) \quad v_{esc} = 310 \text{ km/s} = 3.10 \times 10^5 \text{ m/s}$$

$$\therefore M_G = \frac{R v_{esc}^2}{2G} = \frac{(2.6229 \times 10^{20} \text{ m}) (3.10 \times 10^5 \text{ m/s})^2}{2 \times 6.6726 \times 10^{-11} \text{ Nm}^2/\text{kg}^2} \\ = 1.8888 \times 10^{41} \text{ kg} / 1.989 \times 10^{30} \text{ kg}/M_\odot \\ = 9.5 \times 10^{10} M_\odot \quad (9.4961 \times 10^{10})$$

This value is reasonably close to the value of  $1.25 \times 10^{11} M_\odot$  obtained from assuming Keplerian motion for the LSR about the Galactic centre.

(b) For  $v_{esc} = 500 \text{ km/s} = 5.0 \times 10^5 \text{ m/s}$ , we have:

$$M_G = \frac{R v_{esc}^2}{2G} = \frac{(2.6229 \times 10^{20} \text{ m}) (5.0 \times 10^5 \text{ m/s})^2}{2 \times 6.6726 \times 10^{-11} \text{ Nm}^2/\text{kg}^2} \\ = 4.9136 \times 10^{41} \text{ kg} / 1.989 \times 10^{30} \text{ kg}/M_\odot \\ = 2.5 \times 10^{11} M_\odot \quad (2.4704 \times 10^{11})$$

This value is reasonably close to the value of  $\sim 2 \times 10^{11} M_\odot$  obtained from assuming Keplerian motion for disk stars at 16 kpc from the Galactic centre.

Since Keplerian motion does not apply locally, it seems likely that result (b) may be closer to the true mass of the Galaxy.

4. For Keplerian orbits,  $(M_1 + M_2) = \frac{4\pi^2 a^3}{G P^2}$ , where  $P = \frac{2\pi a}{v}$

$$\therefore (M_1 + M_2) = \frac{4\pi^2 R^3 v^2}{G 4\pi^2 R^2} = \frac{R v^2}{G}, \text{ for } a = R$$

Since  $M_1 = M_G \gg m_2 = m_*$ ,  $\therefore v^2 \approx \frac{G M_G}{R}$

or:  $v = \frac{G^{1/2} M_G^{1/2}}{R^{1/2}}$ , where  $R =$  distance to the Galactic centre,  
 $M_G =$  mass of the Galaxy

$$\therefore \frac{dv}{dR} = \frac{d}{dR} \left( \frac{G^{1/2} M_G^{1/2}}{R^{1/2}} \right) = -\frac{1}{2} \frac{G^{1/2} M_G^{1/2}}{R^{3/2}}$$

$$\text{Oort's A} = -\frac{1}{2} \left[ \left( \frac{dv}{dR} \right)_{R_0} - \frac{v_{R_0}}{R_0} \right] = -\frac{1}{2} \left[ -\frac{1}{2} - 1 \right] \frac{G^{1/2} M_G^{1/2}}{R_0^{3/2}} = \frac{3}{4} \frac{G^{1/2} M_G^{1/2}}{R_0^{3/2}}$$

$$\text{Oort's B} = -\frac{1}{2} \left[ \left( \frac{dv}{dR} \right)_{R_0} + \frac{v_{R_0}}{R_0} \right] = -\frac{1}{2} \left[ -\frac{1}{2} + 1 \right] \frac{G^{1/2} M_G^{1/2}}{R_0^{3/2}} = -\frac{1}{4} \frac{G^{1/2} M_G^{1/2}}{R_0^{3/2}}$$

$$\text{But } \frac{G^{1/2} M_G^{1/2}}{R_0^{3/2}} = \frac{\left[ (6.6726 \times 10^{-11} \text{ N m}^2/\text{kg}^2) (1.989 \times 10^{30} \text{ kg}/M_\odot \times 1.2451 \times 10^{11} M_\odot) \right]^{1/2}}{\left[ (8500 \text{ pc} \times 206265 \text{ AU/pc} \times 1.496 \times 10^{11} \text{ m/AU}) \right]^{3/2}}$$

$$= \frac{\left[ (6.6726 \times 10^{-11} \text{ N m}^2/\text{kg}^2) (1.989 \times 10^{30} \times 1.2451 \times 10^{11} \text{ kg}) \right]^{1/2}}{\left[ 8500 \times 206265 \times 1.496 \times 10^{11} \text{ m} \right]^{1/2}} = 8.5 \text{ kpc}$$

for units in m/s/kpc

$$= \frac{2.51 \times 10^5 \text{ m/s/kpc}}{8.5} = 29.53 \text{ km/s/kpc}$$

$$\therefore A = \frac{3}{4} (29.53 \text{ km/s/kpc}) = 22 \text{ km/s/kpc}$$

$$B = -\frac{1}{4} (29.53 \text{ km/s/kpc}) = -7 \text{ km/s/kpc}$$

Both values lie outside the range of 11-14 km/s/kpc for A and |B| found observationally, implying that Keplerian orbits do not apply in local regions of the Galaxy.

5. For NGC 2281, the best parameters with  $E_{B-V} / A_V = 0.77$  are (see graphs):

$$E_{B-V} = 0.09 \pm 0.01$$

$$V - M_V = 8.70 \pm 0.05 = 5 \log d - 5 + A_V$$

$$\therefore V_0 - M_V = 5 \log d - 5$$

$$V_0 - M_V = V - M_V - A_V = 8.70 - (3 \times 0.09)$$

$$= 8.70 - 0.27$$

$$= 8.43$$

$$\therefore d = 10^{(8.43 + 5)/5} \text{ pc}$$

$$= 485 \text{ pc}$$

$$\frac{\Delta d}{d} = \frac{\Delta(V - M_V)}{2.1714724} = \frac{\pm [(0.05)^2 + (0.03)^2]^{1/2}}{2.1714724} = \pm 0.0583095$$

$$= \pm 0.0268531$$

$$\therefore \Delta d = \pm 0.0268531 \times 485 \text{ pc}$$

$$= \pm 13 \text{ pc}$$

$$\text{i.e. } d = 485 \pm 13 \text{ pc}$$

Hipparcos parallaxes yield (only 3 stars)

Star	$\pi$ (mas)	$\Delta\pi$ (mas)	wgt ( $\frac{1}{\Delta\pi^2}$ )	$\pi \times \text{wgt}$
1	1.63	1.24	0.6503642	1.0600937
2	4.10	1.66	0.3628973	1.4878792
3	0.91	1.40	0.5102040	0.4642857
Sum			1.5234657	3.0122586

$$\therefore \langle \pi \rangle (\text{weighted}) = \frac{3.01 \dots}{1.52 \dots} = 1.9772409 \text{ mas} \pm 0.810184$$

$$\text{Gives } d = 1/\pi = 1/1.977 \text{ pc} = 505.76 \text{ pc} \pm 207.2 \text{ pc (from } \frac{\Delta\pi}{\pi})$$

$$d = 485 \pm 13 \text{ pc (ZAMS fitting) versus } 506 \pm 207 \text{ pc (Hipparcos } \pi\text{s)}$$

ZAMS gives more precise results, although both agree

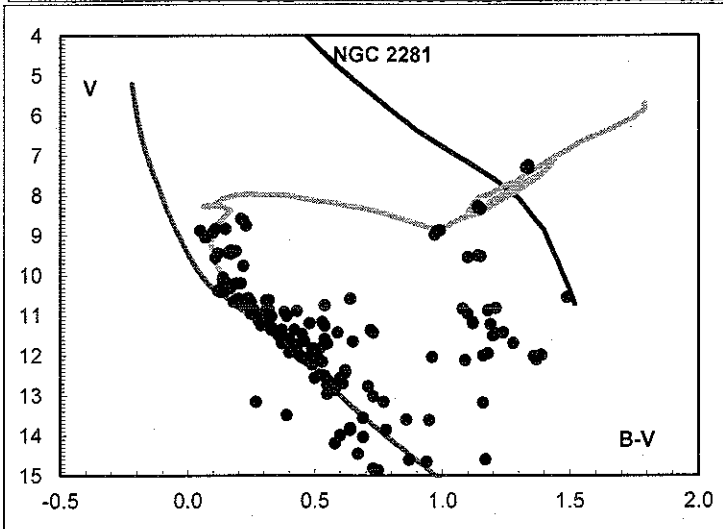
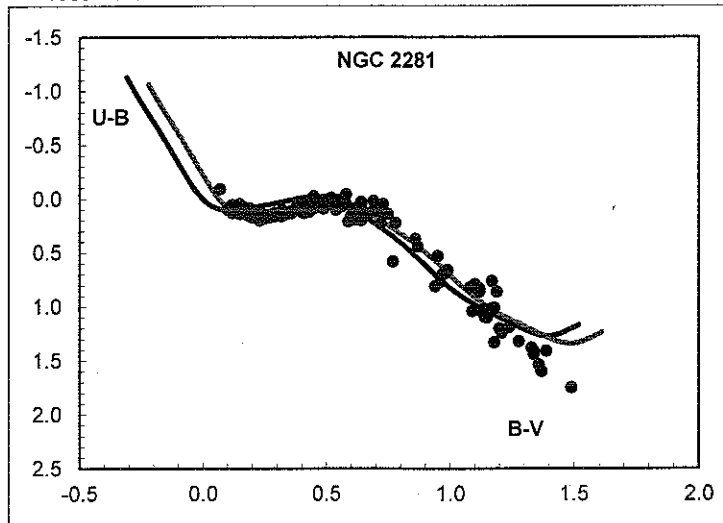
From results for Sica 6 (notes) at similar  $d$ , expect VR (LSR)  $\approx -1 \text{ km/s}$  consistent with observations

RA=06 48 17 174.9  
 DC=+41 04 42 16.88  
 NGC 2281

(B-V)<sub>o</sub> (U-B)<sub>o</sub> M<sub>v</sub> B-V U-B V Eb-v= 0.090 0.01 log t = 8.6  
 V-M<sub>v</sub>= 8.70 0.05 B-V M<sub>v</sub> B-V<sub>red</sub> V<sub>red</sub>  
 Vo-M<sub>v</sub> 8.43 1.70 -3.00 1.790 5.700  
 d= 485 1.70 -2.84 1.790 5.860  
 pm 13 1.65 -2.62 1.740 6.080  
 M<sub>v</sub> -3.09 1.60 -2.47 1.690 6.230  
 dm-M 0.06 1.57 -2.37 1.660 6.330

Star Ref. V B-V U-B

5 1305 11.99 1.39 1.41  
 7 1305 11.74 0.41 0.09



7.00 1.50 -2.18 1.590 6.520  
 7.18 S Sge 1.45 -2.04 1.540 6.660  
 7.35 V 5.614 1.40 -1.83 1.490 6.870  
 7.53 B 6.416 1.35 -1.67 1.440 7.030  
 7.70 U 6.983 1.30 -1.45 1.390 7.250  
 7.87 B-V 0.802 1.25 -1.28 1.340 7.420  
 8.05 U-B 0.567 1.20 -1.04 1.290 7.660  
 8.22 pm 8.38 0.923 1.15 -0.94 1.240 7.760  
 8.38 1.10 -0.74 1.190 7.960  
 8.53 (B-V)<sub>o</sub> 0.7 1.05 -0.65 1.140 8.050  
 8.67 E<sub>bv</sub>(B<sub>0</sub>) -0.76 1.03 -0.52 1.120 8.180  
 8.80 E<sub>b-v</sub> 0.102 1.00 -0.17 1.090 8.530  
 8.93 V<sub>o</sub> 5.344 1.05 -0.24 1.140 8.460  
 9.06 M<sub>v</sub> -3.09 1.10 -0.42 1.190 8.280  
 9.19 1.15 -0.62 1.240 8.080  
 9.31 1.20 -0.79 1.290 7.910  
 9.43 1.25 -1.00 1.340 7.700  
 9.55 1.30 -1.22 1.390 7.480  
 9.65 1.35 -1.58 1.440 7.120  
 9.76 1.30 -1.24 1.390 7.460  
 9.85 1.25 -1.09 1.340 7.610  
 9.95 1.20 -0.91 1.290 7.790  
 10.04 1.15 -0.73 1.240 7.970  
 10.12 1.10 -0.55 1.190 8.150  
 10.20 1.05 -0.40 1.140 8.300  
 10.26 1.00 -0.18 1.090 8.520  
 10.31 0.95 -0.02 1.040 8.680  
 10.36 0.90 0.16 0.990 8.860  
 10.41 0.85 0.08 0.940 8.780  
 10.45 0.80 -0.02 0.890 8.680  
 10.49 0.75 -0.12 0.840 8.580  
 10.54 0.70 -0.23 0.790 8.470  
 10.59 0.65 -0.31 0.740 8.390  
 10.64 0.60 -0.38 0.690 8.320  
 10.69 0.55 -0.43 0.640 8.270  
 10.74 0.50 -0.50 0.590 8.200  
 10.79 0.45 -0.55 0.540 8.150  
 10.84 0.40 -0.58 0.490 8.120  
 10.88 0.35 -0.65 0.440 8.050  
 10.93 0.30 -0.71 0.390 7.990  
 10.97 0.25 -0.72 0.340 7.980  
 11.01 0.20 -0.73 0.290 7.970  
 11.05 0.15 -0.74 0.240 7.960  
 11.09 0.10 -0.71 0.190 7.990  
 11.13 0.05 -0.63 0.140 8.070  
 11.18 0.00 -0.42 0.090 8.280  
 11.21 -0.03 -0.43 0.060 8.270  
 11.25 0.00 -0.46 0.090 8.240  
 11.29 0.05 -0.42 0.140 8.280  
 11.34 0.08 -0.34 0.170 8.360  
 11.39 0.05 -0.15 0.140 8.550  
 11.43 0.03 0.00 0.120 8.700  
 11.48 0.00 0.50 0.090 9.200  
 11.52 0.02 1.00 0.110 9.700  
 11.57 0.05 1.33 0.140 #####  
 11.63 0.10 1.83 0.190 #####  
 11.68 0.15 2.29 0.240 #####  
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 11.78 0.30 0.022 3.08 0.42 0.09 11.78  
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 11.89 0.350 0.013 3.19 0.44 0.08 11.89  
 11.96 0.360 0.008 3.26 0.45 0.08 11.96

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 48 48 11.73 0.42 0.08 0.230 0.068 2.59 0.32 0.14 11.29  
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 48 1305 11.83 0.41 0.06 0.250 0.059 2.69 0.34 0.13 11.39  
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 50 48 11.17 1.12 0.86 0.290 0.041 2.87 0.38 0.11 11.57  
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 50 1305 11.19 1.12 0.83 0.310 0.032 2.98 0.40 0.10 11.68  
 51 48 11.58 0.37 0.10 0.320 0.027 3.03 0.41 0.10 11.73  
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 52 69 10.89 0.43 0.08 0.360 0.008 3.26 0.45 0.08 11.96

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4.551	102.170206	41.066498	32654	06 48 40.85	+41 03 59.5	8.64	102.170218	41.0665167	1.63	-3.79	-7.79	1.24	8.616	0.214	1.63	1.24	0.6504	1.0601
6.8415	101.995275	41.177132	32592	06 47 58.87	+41 10 37.7	10.25	101.995289	41.1771451	4.1	-4.24	-5.3	1.66	10.225	0.162	4.1	1.66	0.3629	1.4879
7.0141	102.092158	40.962527	32626	06 48 22.12	+40 57 45.2	8.86	102.092163	40.9625452	0.91	-1.46	-7.68	1.4	8.834	0.113	0.91	1.4	0.5102	0.4643
																4.3	1.5235	3.0123
															<pi>	1.977		
															unc	0.656		
															d=	506		pc
															unc	168		